

A NEW IMPACT MODIFIER FOR TOUGHENING CLEAR APET

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Abstract

Polymers, as well as glasses, exhibit physical 'aging' which leads to embrittlement. Impact modifier additives counteract this embrittlement. In clear polymer systems, such as amorphous polyethylene terephthalate (APET), blends with typical commercial impact modifiers show a significant loss of optical clarity. The work presented here, based on a new impact modifier additive, shows that embrittlement of APET can be counteracted without significant loss of optical clarity.

Introduction

Physical 'aging' in polymers such as APET has been studied extensively (1-4). Brady (5) showed that impact additives can counteract the embrittlement in polymer systems caused by physical 'aging'.

Typical impact modifier additives such as MBS [methacrylate-butadiene-styrene], ABS [acrylonitrile-butadiene-styrene] and acrylic [butylacrylate based] have refractive indices in the range of 1.52 to 1.54. When they are added to the higher refractive index APET resin (~1.575), they drastically reduce transparency and increase the haze of the blend.

The present work demonstrates that a new, patented (6), core-shell impact additive, Paraloid® EXL-8619, can overcome the embrittlement from 'aging' of APET articles and maintain the desirable optical properties of the articles.

Experimental

'Impact additive'
A novel 'impact additive' based on core-shell chemistry was developed to eliminate the embrittlement of APET and maintain desirable optical properties. The 'impact additive' is a 100 micron powder with refractive index matching that of APET. It can be handled like other typical impact modifiers, e.g. MBS, ABS. It is stable at APET processing conditions. It can be blended into APET without drying.

Blend of APET with 'Impact additive'

The APET resin used for this work was a sheet grade APET with 0.83 dl/gram intrinsic viscosity (IV). The APET pellets were dried under vacuum at 120°C for 16 hours prior to use. The 'impact additive' was not dried. The powder and pellets were blended in the correct ratio and then fed to a twin screw extruder. A 34 mm Leistritz compounding extruder with two counter-rotating, intermeshing screws was used. Barrel temperatures were 255-280-280-280-285°C and melt temperatures of 275-277°C were observed. Screw rpm was set at 168.

An additional set of pellets were prepared by passing them through the Leistritz extruder five (5) times to simulate recycling.

All pellets obtained from the APET / 'impact additive' blends were re-crystallized at 120°C for 3-4 hrs in a tray.

Sheet extrusion

The re-crystallized pellets from the blend were dried at 120°C just prior to sheet extrusion. Clear sheet was extruded from a 38 mm Killion single screw machine with adjustable slit die and then cooled on a roll stack. Barrel temperatures were set at 238-243-243-246°C and the collar and die zones at 246°C. Rpm of the screw was 105. Melt temperatures of 266-267°C were observed. The roll stack was set at 16°C. These conditions gave sheets of 0.8 mm [0.035"] thickness.

Additional sheet samples were prepared from pellets with 'five passes' through the extruder.

Testing

Falling weight impact tests on the sheet materials was run using a DYNATUP instrument. Five tests per sample sheet were measured. Average values for total energy (Joules) and % ductility were reported. A 25.4 mm (1") diameter tup was used as the striking head.

'Aging' of the sheet samples was done in a 60°C air oven for up to 10 days. Samples were allowed to cool to room temperature before testing.

Optical properties of the sheet were measured on a Hunterlab Colorimeter - Illuminant

°C' by ASTM D-1003 method. % luminous transmission and % haze were recorded.

Results and Discussion

Impact after 'aging'

Sheet samples of neat A PET resin and A PET with 5% and 10% 'impact additive' were tested for heat aging resistance. The sheet was 'aged' in a 60°C oven for 1 to 10 days, removed and cooled to room temperature. Table 1 shows the total energy and % ductility measured for A PET sheets with and without the new impact additive. As little as 5% of the new impact additive maintains the impact even after 10 days heat 'aging'.

Recycling is a fact of life for plastics packaging. Thermoformers recycle their trimmed sheet and consumers recycle their food packaging. In order to assess how the modified A PET would handle several recycle passes, a 'worst case' experiment was done: 100% regrind. Additional sheet samples were made with 0, 5 and 10% of the new impact additive, but the pellet compound was re-extruded 5 times in the compounding extruder before make sheet in the Killion extruder. The sheet was 'aged' in a 60°C oven for 1 to 10 days, removed and cooled to room temperature.

Table 2 shows the total energy and % ductility measured for A PET sheets with and without the new impact additive. As expected, all three sheet samples showed lower total energy and % ductility for '5 pass' recycled sheet compared to sheet made in 'one pass' through the extruder. A PET chain scission is the likely cause of the loss of impact.

The neat A PET sheet with '5 passes' through the extruder dropped to 0% ductility at 3 days of heat 'aging'. A PET sheet made with 5% and 10% of the new impact additive survived 10 days heat 'aging' with impact and ductility.

Optical properties

The new, patented, impact additive was designed to maintain the optical properties of A PET while providing impact resistance. Sheets prepared for impact testing were used to measure optical properties such as % luminous transmission and % haze. Table 3 lists these data for A PET sheets made from 'one pass' and 'five pass' [recycle study] pellets. A sheet made from a typical impact modifier at 6% loading in the same A PET is also shown for comparison.

The typical impact modifier gives no luminous transmission and 100% haze even at the low addition level [6%]. The new impact additive lowers the light transmission slightly and increases the haze slightly in comparison to this typical impact additive.

Optical properties for sheets made after '5 passes' through the extruder show less haze than sheets with 'one pass' through the extruder. Dispersion of the impact additive improves with multiple passes through the extruder.

Effect of Moisture from the Impact Additive

It is widely known that A PET and other polyester resins are sensitive to moisture during processing. Drying the A PET to very low H₂O levels, <50 ppm, is necessary to avoid property losses from chain scission. A separate study was run to evaluate the effect of moisture present in the new impact additive on the properties in A PET. Table 4 shows that impact and optical properties of the A PET / impact additive sheets are unaffected by the moisture in the new powder impact additive.

Effect on other properties

This new impact additive has some additional benefits for cutting and de-nesting of modified A PET sheets. These properties will be the subject of future papers.

Conclusions

From data in Tables 1 to 3, it is clear that a new, patented, impact additive allows A PET sheet to retain its impact on 'aging' while maintaining its desirable optical properties.

The residual moisture in the new impact additive does not affect the impact retention on aging or the optical properties in blends made from A PET and the new impact additive.

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Table 1 Impact Properties of Sheet after Thermal Aging at 60°C [total energy (J) and % ductility]

Sample	0 days	1 day	10 days
	J (% D)	J (% D)	J (% D)
APET	36 (100)	31 (80)	12 (60)
" + 5% IA	38 (100)	33 (100)	33 (100)
" + 10% IA	39 (100)	33 (100)	33 (100)

conditions : 25.4 mm (1") tup used in DYNATUP Instrumented Falling Dart ; sheet tested at room temperature ; sheet thickness ~ 0.8mm (0.032"); IA = new 'impact additive'

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Table 2 Impact Properties of Sheet from 5 recycle passes before sheet extrusion Thermal Aging done at 60°C for 1 to 10 days [total energy (J) and % ductility]

Sample	0 days	3 day	10 days
	J (% D)	J (% D)	J (% D)
APET	31 (100)	6 (0)	4 (0)
" + 5% IA	24 (80)	15 (40)	16 (40)
" + 10% IA	28 (100)	25 (100)	22 (80)

conditions : 25.4 mm (1") tup used in DYNATUP Instrumented Falling Dart ; sheet tested at room temperature ; sheet thickness ~ 0.8mm (0.032"); IA = new 'impact additive'

Table 3 Optical Properties of Sheet [% luminous transmission and % haze]

Sample	'one pass' through extruder		'five passes' through extruder	
	% LT	% haze	% LT	% haze
APET	89.4	1.1	88.6	1.3
" + 5% IA	88.6	2.8	87.1	1.7
" + 10% IA	87.6	6.2	87.4	2.8

APET + 6% typical IM * 0 100

conditions : ASTM D 1003 ; Hunterlab Colorimeter ; sheet thickness was 0.8mm (0.032"); IA = new 'impact additive' * the sample of APET with typical IM was run in a different set of experiments

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Table 4 Impact and Optical Properties of APET Sheet made from 'dry' and 'wet' impact additive

Sample	Dynatup Impact 10 days @ 60°C J (% ductility)		Opticals % LT / % haze	
	DRY'	WET'	DRY'	WET'
APET	10 (0)		88.9/0.6	
" + 5% IA	17 (80)	19 (80)	88.6/3.7	88.5/3.5
" + 10% IA	17 (100)	21 (100)	87.7/6.5	87.8/6.1

conditions : 25.4 mm (1") tup used in DYNATUP Instrumented Falling Dart ; sheet tested at room temperature ; sheet thickness ~ 0.8mm (0.032"); IA = new 'impact additive' ; DRY' = 800ppm H2O , WET' = 2500ppm H2O in impact additive powder; IA = new 'impact additive'

KEYWORDS : APET, clarity, aging, additive